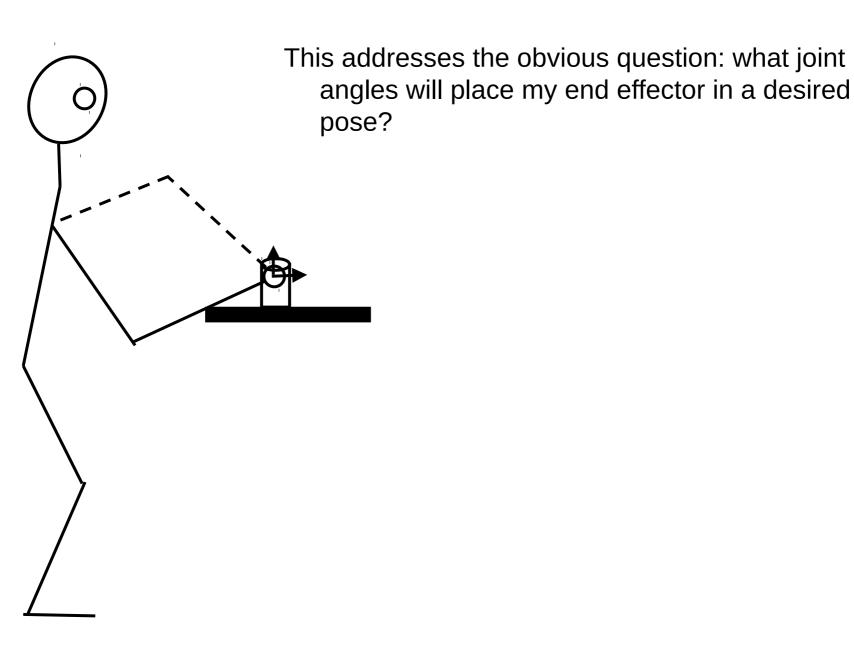
Robert Platt Northeastern University



Closed form (analytical) solution: a sequence or set of equations that can be solved for the desired joint angles

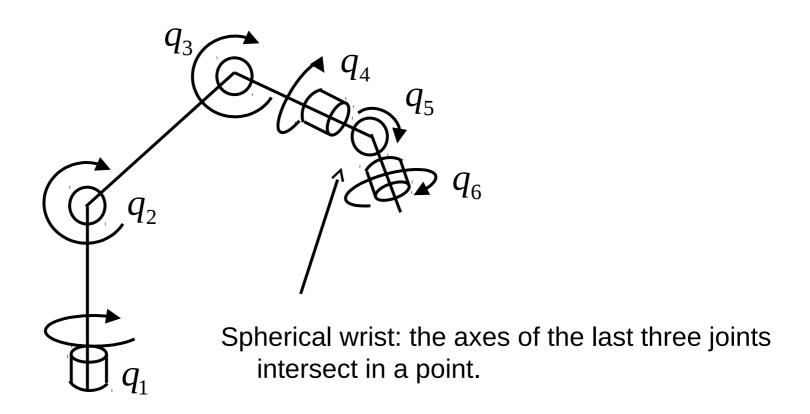
- Potentially faster than an iterative solution
- A unique solution to all manipulator positions can be determined a priori.
  - Can guarantee "safe" joint configurations where the manipulator does not collide with the body.

Iterative (numerical) solution: numerical iteration toward a desired goal position (variation on Newton's method)

- Easier to think about
- Better suited to incremental displacements and control.

### There is no general analytical inverse kinematics solution

- All analytical inverse kinematics solutions are specific to a robot or class of robots.
  - based on geometric intuition about the robot
- I'll give one example there are many variations.



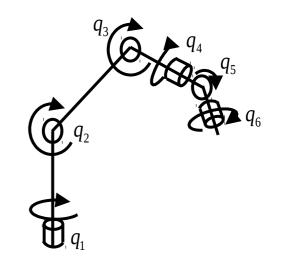
### Consider this 6-joint robot:

this example is out of the book...

#### Problem:

• Given: desired transform, 
$$T_{eff} = \left( egin{array}{cc} R_{eff} & d_{eff} \\ 0 & 1 \end{array} 
ight)$$

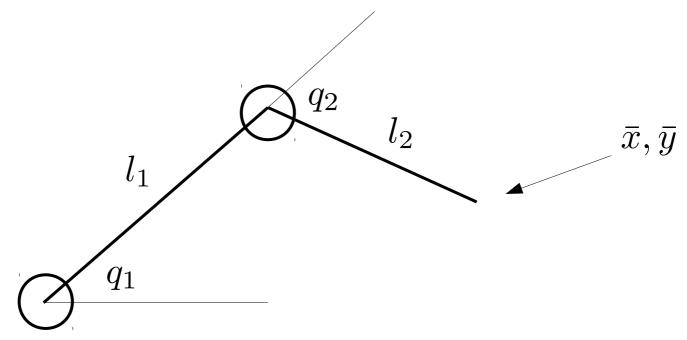
• Find:  $q = (q_1 \quad q_2 \quad q_3 \quad q_4 \quad \cdots \quad q_n)$ 



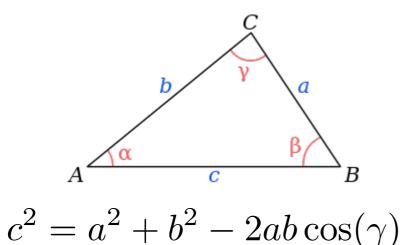
#### Note:

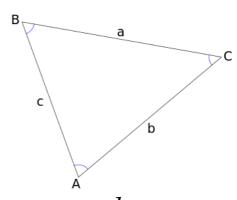
- The desired transform (pose) encodes six degrees of freedom (this info can be represented by six numbers)
  - Since we only have six joints at our disposal, there is no manifold of redundant solutions.
- For this manipulator, the problem can be decomposed into a position component (the first three joints) and an orientation component (the last three joints)
- The first three joints tell you what the position of the spherical wrist

## In class exercise



Given  $l_1$  and  $l_2$  , calculate joint angles that cause eff to reach  $ar{x}, ar{y}$ 

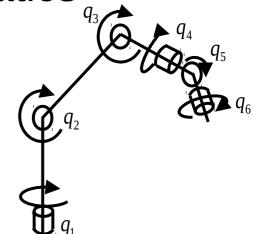




$$\frac{a}{\sin(A)} = \frac{b}{\sin(B)} = \frac{c}{\sin(C)}$$

#### Solution:

First, back out the position of the spherical wrist:

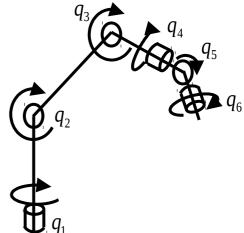


Since it's a spherical wrist, the last three joints can be thought of as rotating about a point.

- A constant transform exists that goes from the last wrist joint out to the end effector (sometimes this is called the "tool" transform):  $^{\it sw}T_{\it eff}$
- Back out the position of the wrist:

$${}^bT_{sw} = {}^bT_{eff} {}^{sw}T_{eff}$$

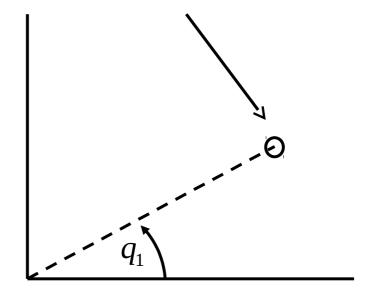
Next, solve for the first three joints



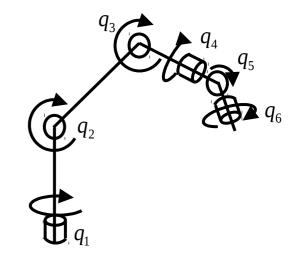
First, solve for  $q_1$ . (look down from above)

$$q_1 = a \tan 2(x_g, y_g)$$
or
$$q_1 = a \tan 2(x_g, y_g) + \pi$$

Goal position in horizontal plane



Next, solve for  $q_3$ . (look at the manipulator orthogonal to the plane of the first two links)



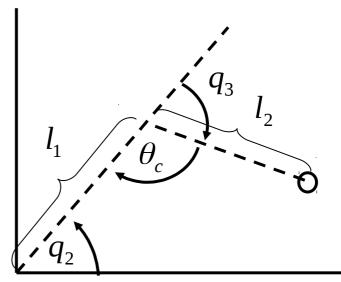
$$c^2 = a^2 + b^2 - 2ab\cos(\theta_c)$$

$$\cos(\theta_c) = \frac{r_g^2 + (z_g - h)^2 - l_1^2 - l_2^2}{2l_1 l_2} = D$$

where  $r_g^2 = x_g^2 + y_g^2$ 

and h is the height of the first link

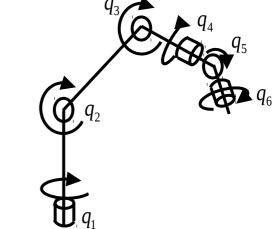
$$\tan(q_3) = \frac{\pm\sqrt{1-D^2}}{D}$$

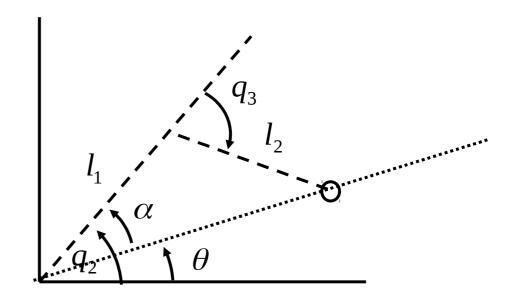


Next, solve for  $q_2$ . (continue to look at the manipulator orthogonal to the plane of the first two links)

$$\tan(\theta) = \frac{z_g - h}{\sqrt{x_g^2 + y_g^2}}$$
$$\tan(\alpha) = \frac{l_2 s_3}{l_1 + l_2 c_3}$$

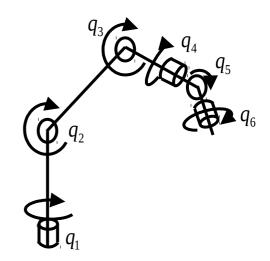
$$q_2 = \theta \pm \alpha$$





Finally, the last three joints completely specify the orientation of the end effector.

- Note that the last three joints look just like ZYZ Euler angles
  - Determination of the joint angles is easy –
    just calculate the ZYZ Euler angles
    corresponding to the desired orientation.



# Remember: ZYZ Euler Angles

$$R_{zyz}(\varphi,\theta,\psi) = \begin{vmatrix} \cos\varphi & -\sin\varphi & 0\\ \sin\varphi & \cos\varphi & 0\\ 0 & 0 & 1 \end{vmatrix} \begin{vmatrix} \cos\theta & 0 & \sin\theta\\ 0 & 1 & 0\\ -\sin\theta & 0 & \cos\theta \end{vmatrix} \begin{vmatrix} \cos\psi & -\sin\psi & 0\\ \sin\psi & \cos\psi & 0\\ 0 & 0 & 1 \end{vmatrix}$$

$$R_{zyz}(\varphi,\theta,\psi) = \begin{vmatrix} c_{\varphi}c_{\theta}c_{\psi} - s_{\varphi}s_{\psi} & -c_{\varphi}c_{\theta}s_{\psi} - s_{\varphi}c_{\psi} & c_{\varphi}s_{\theta} \\ s_{\varphi}c_{\theta}c_{\psi} + c_{\varphi}s_{\psi} & -s_{\varphi}c_{\theta}s_{\psi} + c_{\varphi}c_{\psi} & s_{\varphi}s_{\theta} \\ -s_{\theta}c_{\psi} & s_{\theta}s_{\psi} & c_{\theta} \end{vmatrix}$$

$$\theta = \pm a \tan 2 \left( \sqrt{1 - r_{33}^2}, r_{33} \right)$$

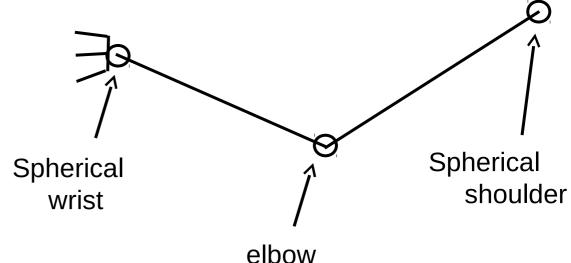
$$\phi = a \tan 2 (r_{23}, r_{13}) + k\pi$$

$$\psi = a \tan 2 (r_{32}, r_{31})$$

## Inverse kinematics for a humanoid arm

You can do similar types of things for a humanoid (7-DOF) arm.

 Since this is a redundant arm, there are a manifold of solutions...



### General strategy:

- 1. Solve for elbow angle
- 2. Solve for a set of shoulder angles that places the wrist in the right position (note that you have to choose an elbow orbit angle)
- 3. Solve for the wrist angles